Grey Gold

Exterior Usage:

Suitable for paving and cladding applications in freezing and non-freezing conditions.

Durability:

Suitable for most commercial and/or high traffic areas. Usage in wet conditions: Suitable for wet surroundings.





Other Names: Ramon Gray Gold Silver Gold Jerusalem Gray Gold Jerusalem Fossil

Stone Type: Limestone

Quarry Location: Mitzpe Ramon, Grebelsky Quarry

Special Notes:

• Application of a sealer is recommended. (Note: It is advised to apply a sealer prior to grouting.)



Test report nº 13-2365-006/E



LAB N°0699

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Date of issue: 28/06/2013

| Sample description | RAMON GREY – GREY GOLD |
|--------------------|---|
| Client | A.Grebelsky & Son (Jerusalem Marble) Company #510234574 4 Hamelacha St. Hartuv A, Industry Zone 99065 Israel |
| provenance | Client's works |
| type of specimen | Natural stone slabs and cubes |
| Sampler | Client |
| Date of sampling | Not declared |
| Date of delivery | 14/04/2013 |
| Number of entrance | 13-2365 |
| Date of entrance | 10/05/2013 |
| test start | 10/05/2013 |
| test end | 28/06/2013 |
| Reference | Initial type testing for CE mark according to EN 1341 :2013 EN 1469 :2004 EN 12057 :2004 EN 12058 :2004 |

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NATURAL STONE TEST METHODS - PETROGRAPHIC EXAMINATION ** (UNI EN 12407:2007)

MACROSCOPIC DESCRIPTION

Natural stone slabs 180 x 90 x 30 mm with sawn surface finish.

Beige fossiliferous sedimentary rock, with heterogeneous structure for the presence of stylolites sometimes opened and compositional patches. There is common presence of bioclasts (bivalves and gastropods).

It is not possible to appreciate micro constituents iso-orientation as well as alteration traces. The rock looks massive, reacts with HCI and can be scratched with a metallic blade as it has a carbonatic origin.



Photo 1: macroscopic look of the POORLY WASHED BIOSPARITE commercially named "Ramon Grey - Grey Gold", (Stereomicroscope 10m)

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MICROSCOPIC DESCRIPTION

Calcareous rock with heterogeneous structure for the presence of stylolites sometimes opened and compositional patches.

The texture is organic- sedimentary with maximum dimensions equal to 4 mm and with granular support.

There are abundant allochemical compounds among which bivalves, gastropods, echinoderms, algae, organogenic scraps. The original aragonite composing most of the bioclasts (bivalves and gastropods) was dissolved and the mould filled with an equant calcite spar cement. Only few original structure of bivalves' shells are preserved.

There are no terrigenous compounds.

Orthochemical compounds are made by sparite, both as coarsely crystalline calcite which filled the mould of the molluscan fragments with dark micritic envelopes, and for fenestral porosity. Opaque minerals as microgranulation are widespread in the section. The micritic matrix, locally re-crystallizing, is heterogeneously widespread.

Discontinuity: they are mainly opened stylolites and micro fractures and also alternatively intergranular pores and fenestral ones.

Alteration: none.

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PHOTOGRAPHIC DOCUMENTATION

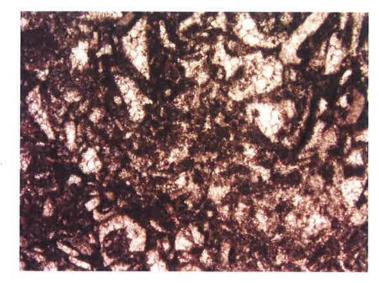


Photo 2: look of the material in thin section. There are a lot of bioclasts mould with dark micritic envelopes and filled with sparite. (25 m. Nicols //).



Photo 3: on the right a fenestral pore calcitized by sparite with micritic lumps inside. On the left calcitic mould of organogenic grit. (25 m. Nicols //).

PETROGRAPHIC DEFINITION (UNI EN 12670:2003):

Commercial definition: Petrographic definition RAMON GREY - GREY GOLD poorly washed biosparite

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DETERMINATION OF WATER ABSORPTION AT ATMOSPHERIC PRESSURE (UNI EN 13755:2008)

| SPECIMEN | specimen dimensions (mm) | | Dry specimen (g) | Saturated specimen (g) | Water absorption (%) | |
|----------|--------------------------|-------------|------------------------|------------------------|----------------------|----------------|
| n. | L | Ľ, | h | m _d | ms | A _b |
| ASS - 1 | 52,8 | 52,8 | 52,1 | 384,23 | 385,31 | 0,3 |
| ASS - 2 | 52,7 | 52,7 | 52,0 | 382,88 | 384,12 | 0,3 |
| ASS - 3 | 52,7 | 52,6 | 52,2 | 383,64 | 384,85 | 0,3 |
| ASS - 4 | 52,8 | 52,7 | 51,7 | 382,61 | 383,85 | 0,3 |
| ASS - 5 | 52,9 | 51,8 | 52,7 | 383,20 | 384,27 | 0,3 |
| ASS - 6 | 52,7 | 51,8 | 52,9 | 383,79 | 384,90 | 0,3 |
| | mea | in water ab | sorption (% |) | | 0,3±0,1 |

Note: extended uncertainty of the mean value has been calculated with a coverage factor k = 2,57 corresponding to a confidence level of 95 %

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DETERMINATION OF APPARENT DENSITY (UNI EN 1936:2007) *

| specimen | dry specimen (g) | saturated specimen (g) | immersed specimen (g) | Apparent density (kg/m³) |
|----------|------------------|---------------------------|--------------------------|-----------------------------|
| ASS - 1 | 384,23 | 385,63 | 242,26 | 2674,6 |
| ASS - 2 | 382,88 | 384,51 | 241,29 | 2668,0 |
| ASS - 3 | 383,64 | 385,01 | 241,77 | 2672,9 |
| ASS - 4 | 382,61 | 383,97 | 241,17 | 2674,0 |
| ASS - 5 | 383,20 | 384,66 | 241,67 | 2674,5 |
| ASS - 6 | 383,79 | 385,17 | 242,04 | 2676,0 |
| | Mean app | arent density (kg/r | n ³) | 2670 |

DETERMINATION OF OPEN POROSITY (1936:2007)*

| specimen | dry specimen (g) | saturated specimen (g) | immersed specimen (g) | Open porosity (%) |
|----------|------------------|---------------------------|--------------------------|-------------------|
| ASS - 1 | 384,23 | 385,63 | 242,26 | 1,0 |
| ASS - 2 | 382,88 | 384,51 | 241,29 | 1,1 |
| ASS - 3 | 383,64 | 385,01 | 241,77 | 1,0 |
| ASS - 4 | 382,61 | 383,97 | 241,17 | 1,0 |
| ASS - 5 | 383,20 | 384,66 | 241,67 | 1,0 |
| ASS - 6 | 383,79 | 385,17 | 242,04 | 1,0 |
| | Mean o | open porosity (%) | | 1,0 |

HYGROTHERMAL PROPERTIES - TABULATED DESIGN VALUES (UNI EN ISO 10456 :2008)*

| $\begin{array}{c} \textbf{APPARENT}\\ \textbf{DENSITY} \ \rho \ (\text{kg/m}^3)^1 \end{array}$ | Thermal conductivity λ w/(mK) |
|--|----------------------------------|
| 2670 | 2,3 |

¹mean apparent density

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Test report n° 13-2365-006/E

Date of issue: 28/06/2013

DETERMINATION OF FLEXURAL STRENGTH UNDER CONCENTRATED LOAD (UNI EN 12372:2007)

- Load rate: 0,25 MPa/s -
- Surface finish: sawn # -
- Load orientation: perpendicolular to the utilization plane -

| n. | L | Supporting distance (/) | b | h | F | R _{TF} |
|--------|----------|-------------------------|-----------|------|------|-----------------|
| F - 1 | 182,6 | 150,5 | 91,1 | 31,3 | 5229 | 13,2 |
| F - 2 | 182,6 | 150,5 | 91,1 | 29,0 | 4753 | 14,0 |
| F - 3 | 181,7 | 150,5 | 91,0 | 29,9 | 5061 | 14,0 |
| F - 4 | 180,2 | 150,5 | 91,1 | 30,2 | 4096 | 11,1 |
| F - 5 | 182,3 | 150,5 | 91,2 | 32,6 | 4921 | 11,5 |
| F-6 | 182,4 | 150,5 | 90,4 | 28,3 | 4003 | 12,5 |
| F - 7 | 181,9 | 150,5 | 91,3 | 30,6 | 4436 | 11,7 |
| F - 8 | 182,4 | 150,5 | 90,8 | 28,4 | 4796 | 14,8 |
| F - 9 | 180,6 | 150,5 | 91,1 | 30,1 | 4558 | 12,5 |
| F - 10 | 180,3 | 150,5 | 90,8 | 30,9 | 4594 | 12,0 |
| | Mean fle | exural streng | ht (MPa): | | | 12,7 |

| Number of specimen | 10 |
|--------------------------------|--------------|
| Mean Value (MPa) | 12,7 ±0,8MPa |
| Standard deviation | 1,23 |
| Coefficient of variation | 0,10 |
| Mean logarithmic | 2,54 |
| Logarithmic standard deviation | 0,095 |
| Minimum value (MPa) | 11,1 |
| Maximum value (MPa) | 14,8 |
| Lower expected value (MPa) | 10,4 |
| Quantile factor K _S | 2,10 |

NOTE: the extended uncertainty of the mean value has been calculated with a coverage factor k = 2,09, corresponding to a confidence level of 95 %

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Date of issue: 28/06/2013

DETERMINATION OF FLEXURAL STRENGTH UNDER CONCENTRATED LOAD (UNI EN 12372:2007) (after freeze/thaw cycles according to UNI EN 12371:2010)*

- Load rate: 0,25 MPa/s -
- Number of cycles: 56 -
- Visual inspection after freeze/thaw cycles: very minor damage (minor rounding of corners and edges) wich does not compromise the integrity of the specimen.
- Surface finish#: sawn -
- Load orientation: perpendicolular to the utilization plane -

| specimen | | Dimensio | Breaking load (N) | Flexural strength (MPa) | | |
|----------|---------|-------------------------|----------------------|-------------------------------|------|-----------------|
| n. | L | Supporting distance (/) | b | h | F | R _{TF} |
| F - 1 | 182,3 | 150,5 | 91,1 | 31,1 | 5409 | 13,9 |
| F - 2 | 182,2 | 150,5 | 91,0 | 31,0 | 5234 | 13,5 |
| F-3 | 182,1 | 150,5 | 91,1 | 30,5 | 5050 | 13,5 |
| F - 4 | 181,7 | 150,5 | 91,0 | 31,6 | 4133 | 10,3 |
| F-5 | 180,3 | 150,5 | 91,2 | 30,5 | 4989 | 13,3 |
| F-6 | 181,2 | 150,5 | 91,3 | 31,7 | 4271 | 10,5 |
| F - 7 | 181,7 | 150,5 | 91,4 | 28,0 | 4280 | 13,5 |
| F-8 | 180,3 | 150,5 | 91,1 | 29,2 | 4839 | 14,1 |
| F - 9 | 179,8 | 150,5 | 91,2 | 28,6 | 4326 | 13,1 |
| F - 10 | 179,9 | 150,5 | 91,0 | 28,5 | 3325 | 10,2 |
| | Mean fl | exural streng | ht (MPa): | | | 12,6 |

| Number of specimen | 10 |
|--------------------------------|------------|
| Mean Value (MPa) | 12,6 ±1MPa |
| Standard deviation | 1,58 |
| Coefficient of variation | 0,13 |
| Mean logarithmic | 2,52 |
| Logarithmic standard deviation | 0,134 |
| Minimum vale (MPa) | 10,2 |
| Maximum value (MPa) | 14,1 |
| Lower expected value (MPa) | 9,4 |
| Quantile factor K _s | 2,10 |

NOTE: the extended uncertainty of the mean value has been calculated with a coverage factor k = 2,09, corresponding to a confidence level of 95 %

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Mean flexural strenght (R_{TF}) before freeze/thaw cycles:

R_{TF}: 12,7 MPa

Mean flexural strenght (RTF) after freeze/thaw cycles:

R_{TF}: 12,6 MPa

The mean value of flexural strenght is not decreased more than 20 % after the freeze/thaw cycles.

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Test report n° 13-2365-006/E

Date of issue: 28/06/2013

DETERMINATION OF THE BREAKING LOAD AT DOWEL HOLE (UNI EN 13364:2003)*

Key

| symbol | description | | | | | |
|--------|---|--|--|--|--|--|
| d1 | distance from the hole to the face in the direction of the force in (mm), approximate to 1,0 mm | | | | | |
| ba | maximum distance of the centre of the hole to the fracture edges in (mm), approximate to 1,0 mm | | | | | |
| F | Breaking load, in Newton, approximate to 50 N | | | | | |

| TEST CHARACTERISTIC | | | | | | |
|----------------------|------|--|--|--|--|--|
| TEST TYPE: | 0 | | | | | |
| HOLE DIAMETER (mm): | 10,0 | | | | | |
| DOWEL DIAMETER (mm): | 6,1 | | | | | |

| Specimen N. | L1 | L2 | d | Point N. | d (mm) | d₁ (mm) | b _a (mm) | F (N) |
|-------------|-------|-------|------|----------|-------------|---------------------|---------------------|-------|
| | 100.4 | | · | 1 | 30,6 | 11 | 55 | 1550 |
| | | 199,5 | 30,9 | 2 | 30,8 | 11 | 51 | 1950 |
| 1 | 198,4 | 199,0 | 30,9 | 3 | 30,6 | 11 | 35 | 1650 |
| | | | | 4 | 31,7 | 12 | 55 | 1850 |
| | | | | N | lean Value: | 11 | 49 | 1750 |
| Specimen N. | L1 | L2 | d | Point N. | d (mm) | d ₁ (mm) | b _a (mm) | F (N) |
| | | 205,2 | 32 | 1 | 32,0 | 10 | 40 | 1250 |
| | 203 | | | 2 | 32,0 | 10 | 41 | 1600 |
| 2 | | | | 3 | 32,1 | 12 | 38 | 1700 |
| | | | | 4 | 32,0 | 11 | 34 | 1650 |
| | | | | N | lean Value: | 11 | 38 | 1550 |
| Specimen N. | L1 | L2 | d | Point N. | d (mm) | d₁ (mm) | b _a (mm) | F (N) |
| | | | | 1 | 31,4 | 11 | 39 | 1500 |
| | 100.9 | 199 | 24.5 | 2 | 31,6 | 10 | 40 | 1100 |
| 3 | 199,8 | 199 | 31,5 | 3 | 31,4 | 12 | 52 | 2000 |
| | | | | 4 | 31,5 | 11 | 41 | 1600 |
| | | | | N | lean Value: | 11 | 43 | 1550 |

| 12 |
|------|
| 1617 |
| 260 |
| 0,16 |
| 7,38 |
| 0,17 |
| 1100 |
| 2000 |
| 1130 |
| 2,06 |
| |

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| Specimen N° | groove Lenght ¹ (mm) | |
|-------------|---------------------------------|--|
| A - 1 | 25,5 | |
| A - 2 | 23,5 | |
| A - 3 | 26,0 | |
| A - 4 | 23,5 | |
| A - 5 | 23,5 | |
| A - 6 | 25,5 | |
| Mean Value | 24,5 | |

DETERMINATION OF THE ABRASION RESISTANCE (UNI EN 14157:2005)* Method A - Wide wheel abrasion test

SURFACE FINISH#: SAWN

¹NOTE: groove lenght already corrected joining the calibration factor of 0,4 mm.

DETERMINATION OF THE SLIP RESISTANCE VALUE BY MEANS OF THE PENDULUM TESTER (UNI EN 14231:2004) (USRV)*

| Specimen N° | Mean of the two recorded values measured in opposite directions (USRV) |
|-------------|--|
| S - 1 | 43 |
| S - 2 | 55 |
| S - 3 | 48 |
| S - 4 | 52 |
| S - 5 | 49 |
| S - 6 | 45 |
| Mean Value | 49 |

Slider lenght: 76 mm •

Surface finish#: sawn

Slider and sampling « wet »

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DETERMINATION OF THE SLIP RESISTANCE VALUE BY MEANS OF THE PENDULUM TESTER (UNI EN 14231:2004) (SRV)*

- Slider Length: 76 mm
- Surface finish[#]: honed
- Slider and specimen condition: "dry"

| Specimen N° | Average value ¹ (SRV "dry") |
|---------------|---|
| 1 | 44 |
| 2 | 45 |
| 3 | 44 |
| 4 | 51 |
| 5 | 47 |
| 6 | 48 |
| Average value | 47 |

- Slider Length: 76 mm .
- Surface finish[#]: honed
- Slider and specimen condition : "wet"

| Specimen N° | Average value ¹ (SRV ''wet'') |
|---------------|---|
| 1 | 6 |
| 2 | 6 |
| 3 | 8 |
| 4 | 15 |
| 5 | 10 |
| 6 | 10 |
| Average value | 9 |

The TRL pendulum tester has a range of reading from 0 to 150, high values indicate good slip resistance.

¹Note: mean value of 5 + 5 individual measurement obtained with orientation A and A to 180°

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Test report n° 13-2365-006/E

Date of issue: 28/06/2013

13/16 DETERMINATION OF THE SLIP RESISTANCE VALUE BY MEANS OF THE PENDULUM TESTER (UNI EN 14231:2004) (SRV)*

- Slider Length: 76 mm
- Surface finish[#]: heavy patina
- Slider and specimen condition: "dry"

| Specimen N° | cimen N° Average value ¹ (SRV "dry") | |
|---------------|--|--|
| 1 | 44 | |
| 2 | 45 | |
| 3 | 46 | |
| 4 | 47 | |
| 5 | 47 | |
| 6 | 48 | |
| Average value | 46 | |

- Slider Length: 76 mm
- Surface finish#: heavy patina
- Slider and specimen condition : "wet"

| Specimen N° | Average value ¹ (SRV ''wet'') |
|---------------|---|
| 1 | 15 |
| 2 | 10 |
| 3 | 14 |
| 4 | 13 |
| 5 | 12 |
| 6 | 15 |
| Average value | 13 |

The TRL pendulum tester has a range of reading from 0 to 150, high values indicate good slip resistance.

¹Note: mean value of 5 + 5 individual measurement obtained with orientation A and A to 180°

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DETERMINATION OF THE SLIP RESISTANCE VALUE BY MEANS OF THE PENDULUM TESTER (UNI EN 14231:2004) (SRV)*

- Slider Length: 76 mm
- Surface finish[#]: tumbled
- Slider and specimen condition: "dry"

| Specimen N° | Average value ¹ (SRV "dry") | |
|---------------|---|--|
| 1 | 61 | |
| 2 | 58 | |
| 3 | 60 | |
| 4 | 57 | |
| 5 | 59 | |
| 6 | 62 | |
| Average value | 60 | |

- Slider Length: 76 mm
- Surface finish[#]: tumbled
- Slider and specimen condition : "wet"

| Specimen N° | N° Average value ¹ (SRV "wet") | |
|---------------|--|--|
| 1 | 42 | |
| 2 | 37 | |
| 3 | 33 | |
| 4 | 34 | |
| 5 | 35 | |
| 6 | 38 | |
| Average value | 37 | |

The TRL pendulum tester has a range of reading from 0 to 150, high values indicate good slip resistance.

¹Note: mean value of 5 + 5 individual measurement obtained with orientation A and A to 180°

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DETERMINATION OF THE SLIP RESISTANCE VALUE BY MEANS OF THE PENDULUM TESTER (UNI EN 14231:2004) (SRV)*

- Slider Length: 76 mm •
- Surface finish[#]: stardust
- Slider and specimen condition: "dry"

| Specimen N° | ecimen N° Average value ¹ (SRV "dry") | |
|---------------|---|--|
| 1 | 80 | |
| 2 | 72 | |
| 3 | 75 | |
| 4 | 70 | |
| 5 | 71 | |
| 6 | 72 | |
| Average value | 73 | |

- Slider Length: 76 mm
- Surface finish[#]: stardust
- Slider and specimen condition : "wet"

| Specimen N° | Average value ¹ (SRV "wet") 65 | |
|---------------|---|--|
| 1 | | |
| 2 | 63 | |
| 3 | 62 | |
| 4 | 62 | |
| 5 | 63 | |
| 6 | 64 | |
| Average value | 63 | |

The TRL pendulum tester has a range of reading from 0 to 150, high values indicate good slip resistance.

¹Note: mean value of 5 + 5 individual measurement obtained with orientation A and A to 180°

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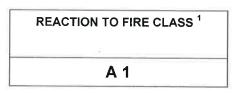
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DECLARATION OF REACTION TO FIRE CLASS (UNI EN 13501-1:2007)*



¹according to Commission Decision n° 96/603/EC.

DETERMINATION OF RESISTANCE TO AGING BY THERMAL SHOCK (UNI EN 14066:2004)* - evaluation of change in mass after the cycles -

Cycle description: specimens are heated at 105°C for 18 h and immediately immerged in water at 20°C for 6 h. The total number of cycles are 20.

| specimen n° | m₀ (g) | m _f (g) | ∆m (%) | vioual departation |
|-------------|--------|--------------------|---------|-----------------------------------|
| opconnon n | | | ΔΠ (70) | visual description |
| 1 | 2080,8 | 2080,4 | 0,0 | not appreciable alteration traces |
| 2 | 2071,7 | 2071,0 | 0,0 | not appreciable alteration traces |
| 3 | 2080,9 | 2080,3 | 0,0 | not appreciable alteration traces |
| 4 | 2082,4 | 2081,8 | 0,0 | not appreciable alteration traces |
| 5 | 2151,0 | 2150,5 | 0,0 | not appreciable alteration traces |
| 6 | 2140,3 | 2139,9 | 0,0 | not appreciable alteration traces |
| | | Mean Value (%) | 0,0 | |

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m₀ (g) = mass of dried specimen before the test m_f (g) = mass of dried specimen after the test Δm (%) = mass change after the cycles

Geotechnical Division The Director Dr. Geologist Francesco Bazzolo

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